

Innovative design with bi-level topology optimization

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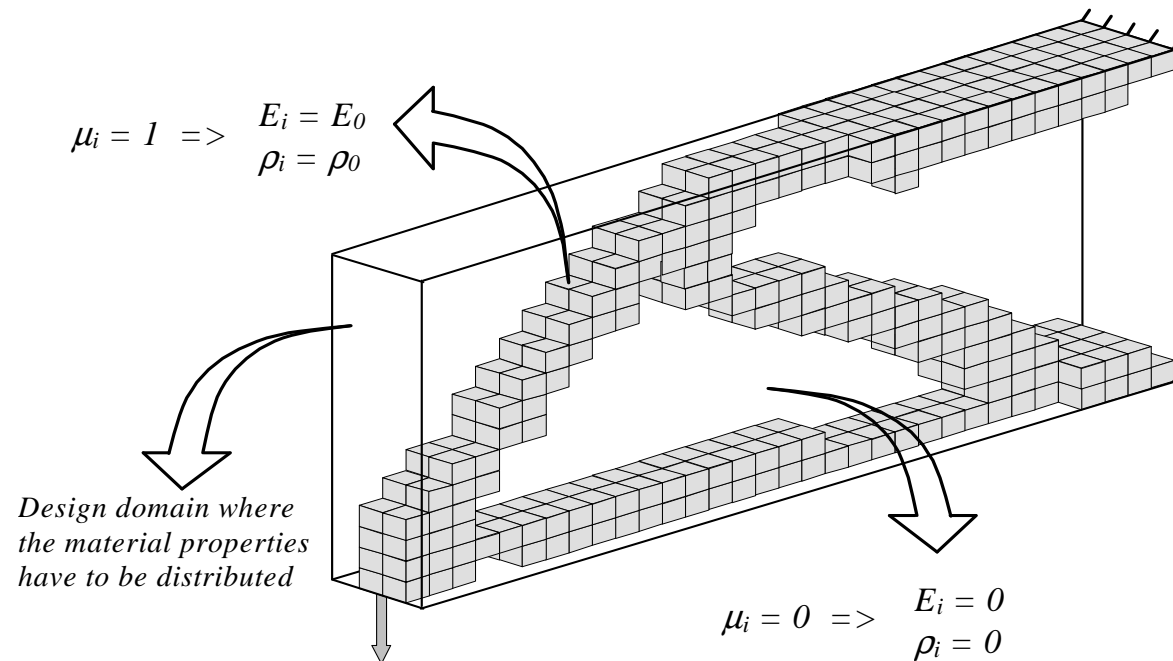
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1st EASN Association Workshop on Aerostructures
October 7-8, Paris, France

- TOPOL software for topology optimization
- Original design of Airbus pylons
- Formulation of a bi-level optimization including TOPOL
- Application
- Conclusions

Classical formulation: maximize stiffness of the structure for a given volume fraction of material required at solution.



μ_i = design variable associated to each finite element i (**pseudo-density**)

{	$\mu_i \approx 0$	Void at the solution in finite element i
	$\mu_i = 1$	Material at the solution in finite element i

Classical formulation: maximize stiffness of the structure for a given volume fraction of material required at solution.

For the linear case:

$$\max_{\boldsymbol{\mu}} \min_{k=1,\dots,nf} \omega_k \quad \text{with} \quad (\mathbf{K} - \omega_k^2 \mathbf{M}) \mathbf{q}_k = 0 \quad \text{Modal analysis}$$

$$\min_{\boldsymbol{\mu}} \max_{l=1,\dots,nc} C_l = \mathbf{g}_l^T \mathbf{q}_l \quad \text{with} \quad \mathbf{K} \mathbf{q}_l = \mathbf{g}_l \quad \text{Linear static analysis}$$

$$\tilde{q}_j \leq \bar{q} \quad \text{Bounded displacement at node } j$$

$$\sum_i \mu_i V_i \leq \bar{V} \quad \text{Bounded volume}$$

$$0 < \underline{\mu}_i \leq \mu_i \leq 1 \quad \text{Side constraints}$$

$$\boldsymbol{\mu} = \{\mu_i, i = 1, \dots, n\}$$

Classical formulation: maximize stiffness of the structure for a given volume fraction of material required at solution.

For the linear case:

When only displacement constraints are taken into account:

$$\min_{\mu} V \quad \text{with} \quad \mathbf{K} \mathbf{q}_l = \mathbf{g}_l \quad \text{Linear static analysis}$$

$$\tilde{q}_j \leq \bar{q} \quad \text{Bounded displacement at node } j$$

Material law: SIMP => specific parameterization of the material properties

- Mass density

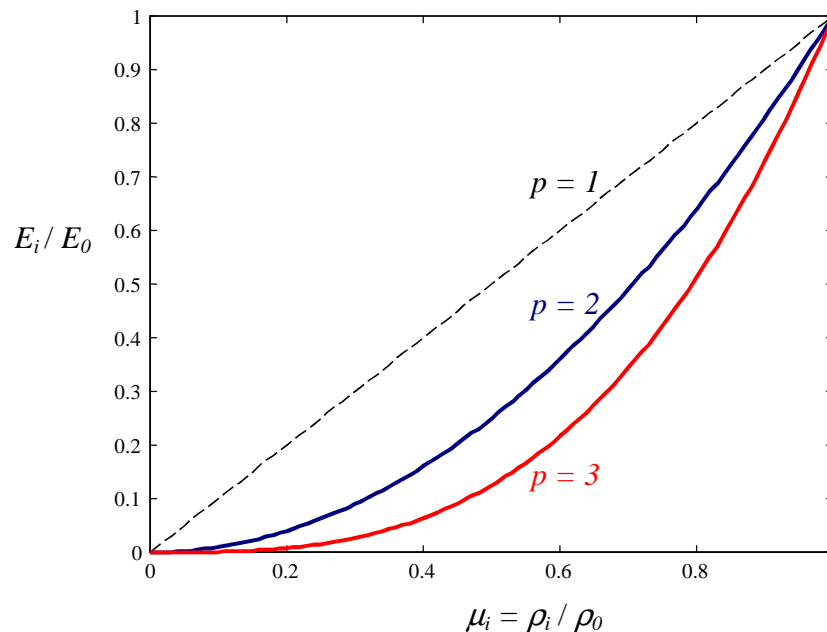
$$\rho_i = \mu_i \times \rho_0$$

Base material properties
(e.g. aluminium)

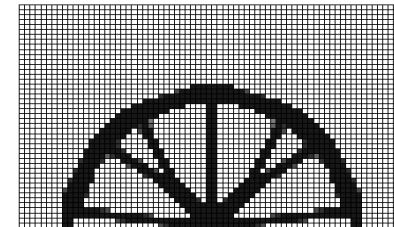
- Young modulus

$$E_i = \mu_i^p E_0$$

$p > 1 \rightarrow$ to penalize intermediate densities



Goal = to have a “black-and-white” final design

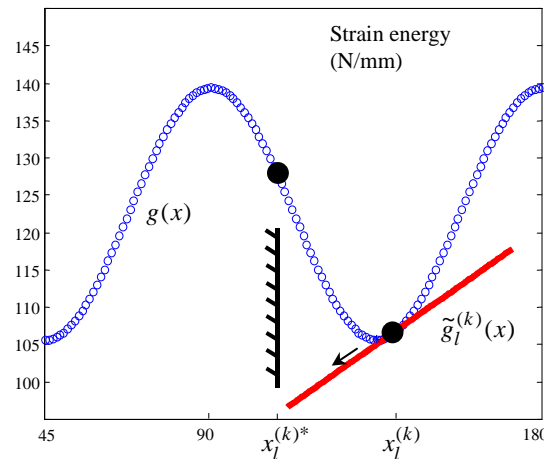


Optimisation algorithm

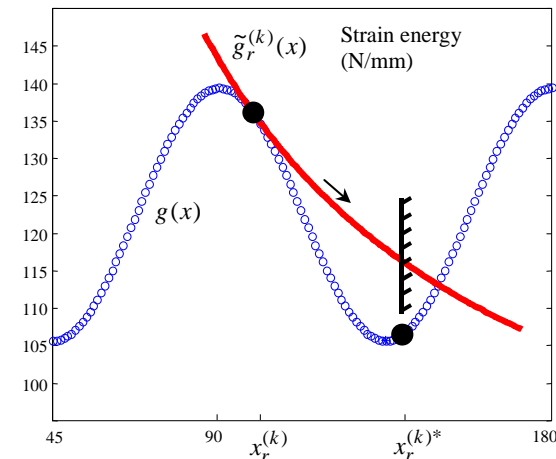
- **Sequential Convex Programming method**

- Details:

- Based on **CONLIN** (Fleury and Braibant, *Int. J. Num. Meth. Engng.*, 1986)
- Generate successive approximations of the initial optimization problem
- multi-objective formulation (*min max* or *max min*)
- dual solver



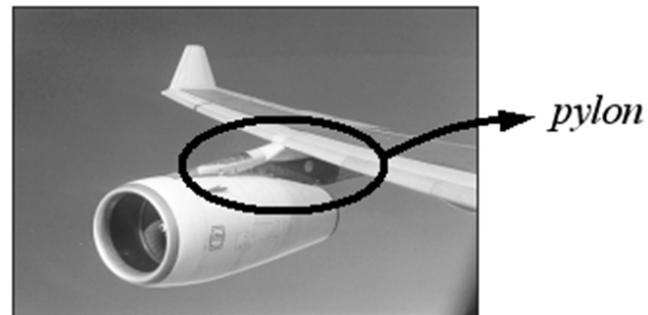
Automatic selection



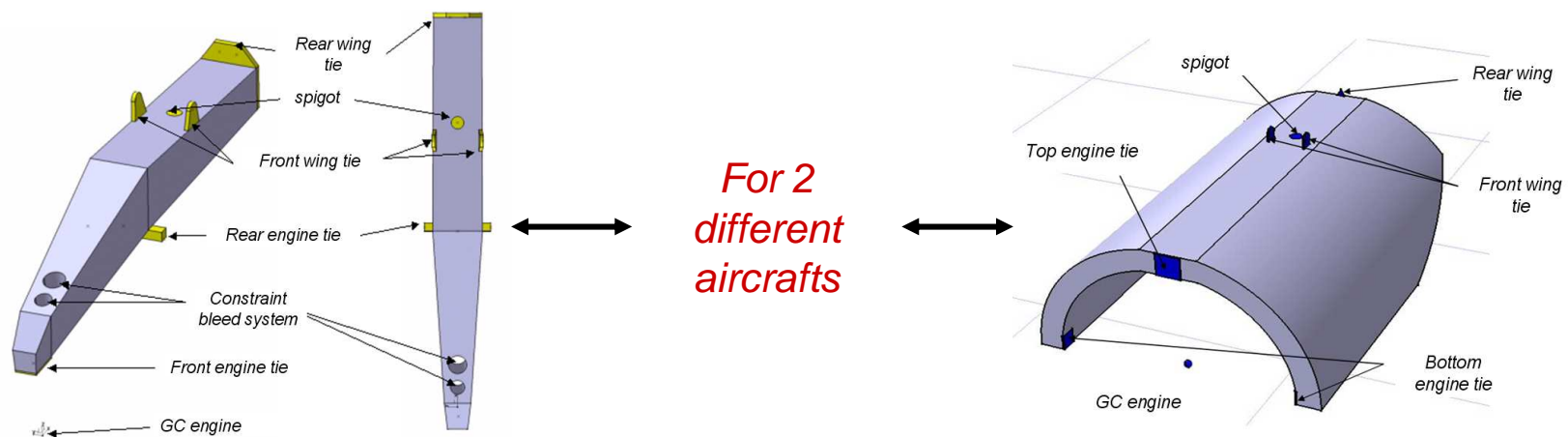
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Original designs of Airbus pylons

The structure to optimize

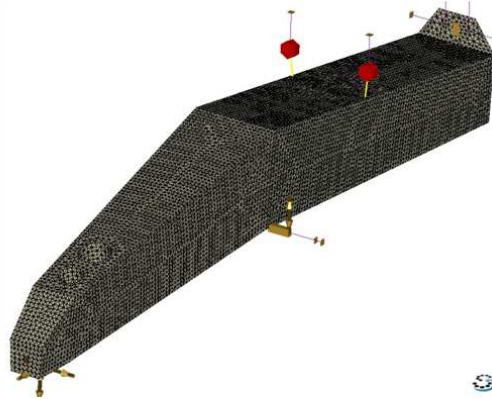


Two enveloppes for the design



Original designs of Airbus pylons

The first design



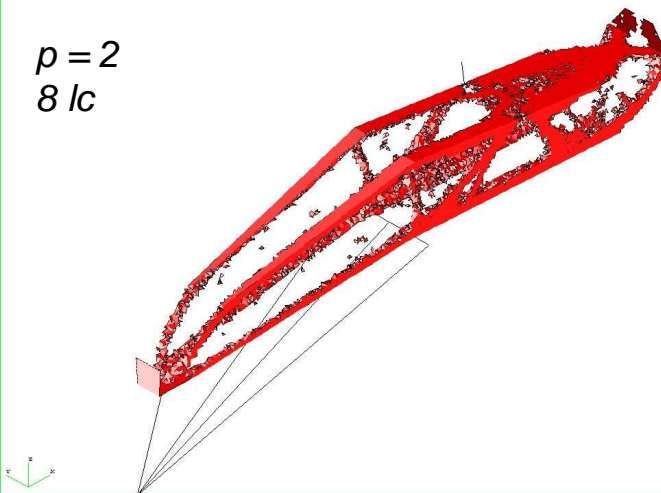
- Number of tetrahedral elements
= Number of design variables = 244021
- 8 static load cases (maneuvers, gust, fan blade off, landing on the engine) + 2 bounded displacements

$$\min_{\mu} \max_{l=1,\dots,8} C_l = \mathbf{g}_l^T \mathbf{q}_l \quad \text{with} \quad \sum_i \mu_i V_i \leq 0.1$$

$$\tilde{q}_j \leq \bar{q}$$

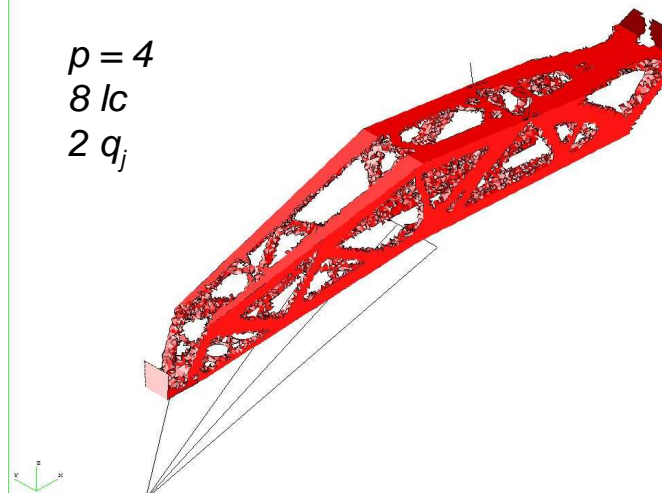
Topology Optimization - iapa2FSYM_GFW
IAPA2 : Loads GUST FBO WUL SYMMETRIC

$p = 2$
 $8 \text{ } l_c$



Topology Optimization - ...4SYM_UNIYZGFW
IAPA2 : Loads GUST FBO WUL UNIY UNIZ SYMMETRIC

$p = 4$
 $8 \text{ } l_c$
 $2 \text{ } q_j$

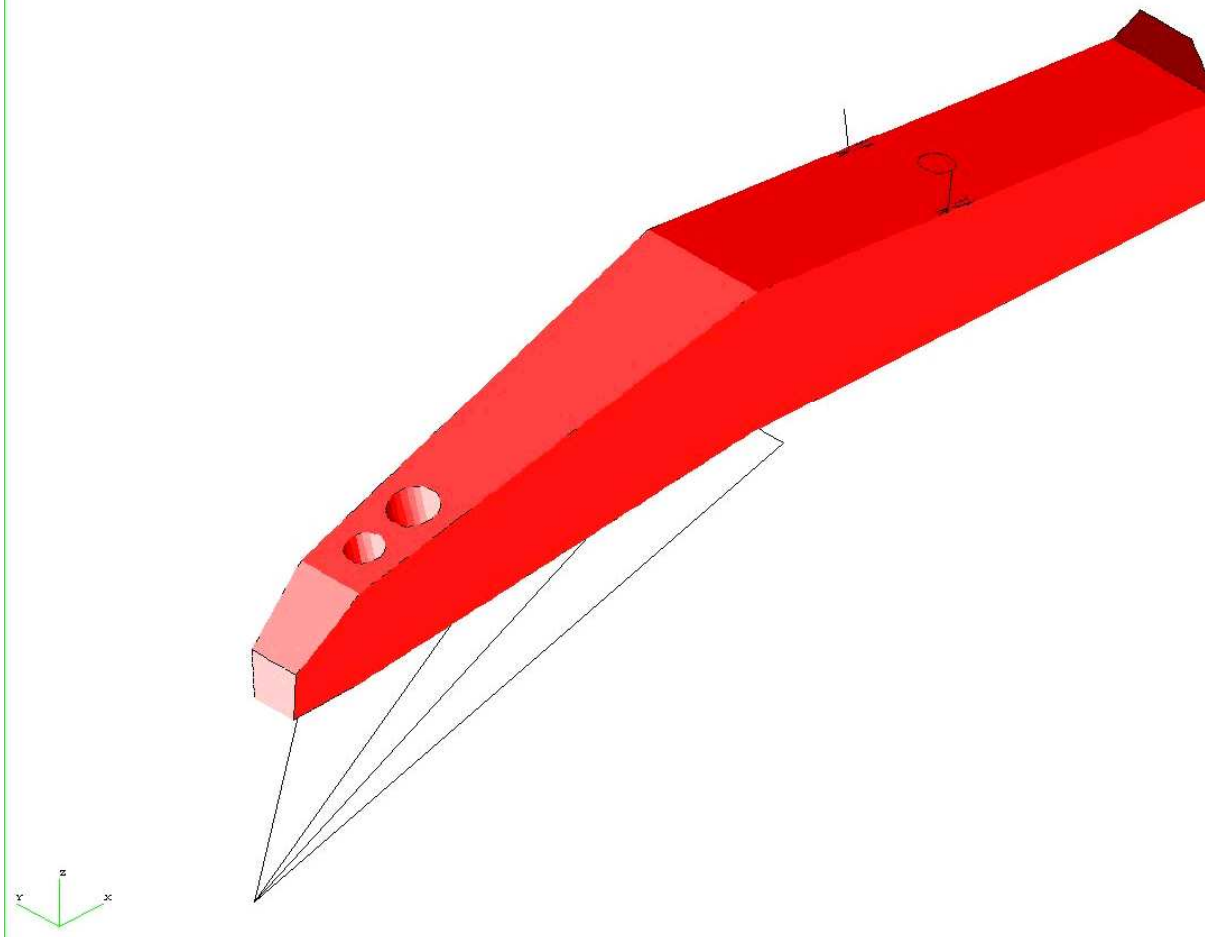


Original designs of Airbus pylons

The first design

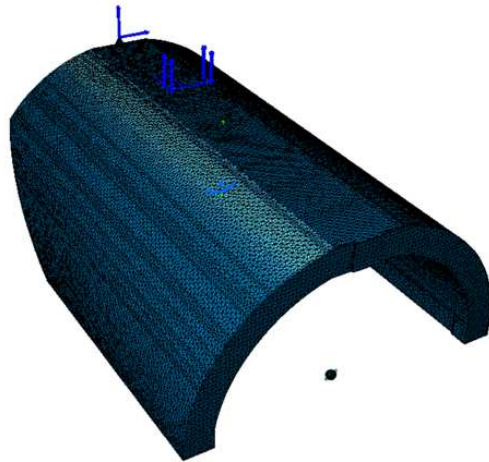
Topology Optimization - ...YM_UNIYZGFW01

IAPA2 : Loads GUST FBO WUL UNIY UNIZ SYMMETRIC



Original designs of Airbus pylons

The second design



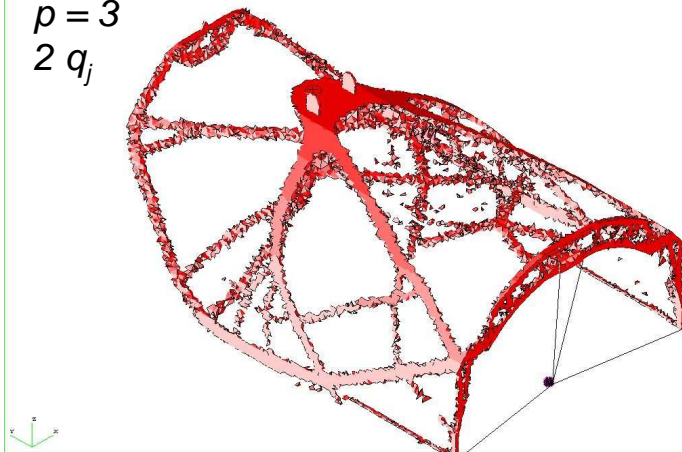
- Number of tetrahedral elements
= Number of design variables = 420839
- 8 static load cases (maneuvers, gust, fan blade off, landing on the engine) + 2 bounded displacements

$$\min_{\mu} \max_{l=1,\dots,8} C_l = \mathbf{g}_l^T \mathbf{q}_l \quad \text{with} \quad \sum_i \mu_i V_i \leq 0.1$$

$$\tilde{q}_j \leq \bar{q}$$

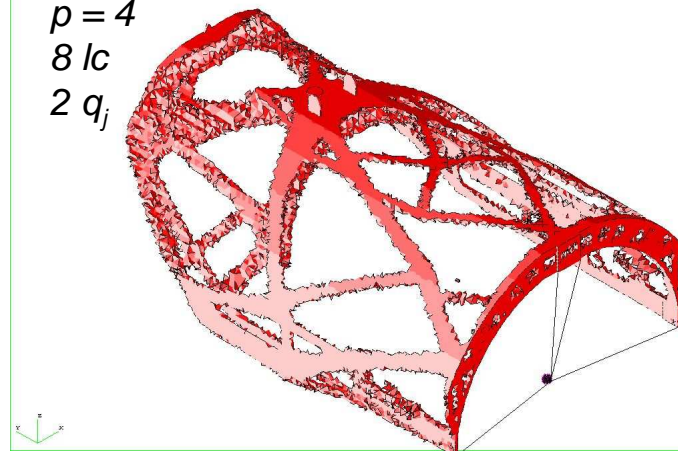
Topology Optimization - ...lot2_P3UNIYZ
IAPA2 : Loads UNIZ UNIZ SYMMETRIC

$p = 3$
 $2 q_j$



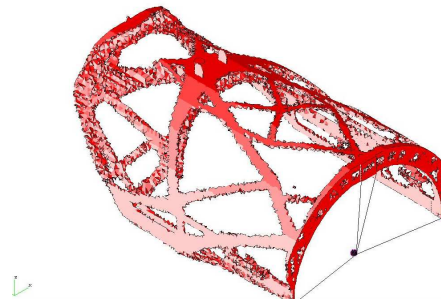
Topology Optimization - ...t2_P4GFWUNIYZ
IAPA2 : Loads GUST FBO WUL UNIZ UNIZ SYMMETRIC

$p = 4$
 $8 l_c$
 $2 q_j$



Original designs of Airbus pylons

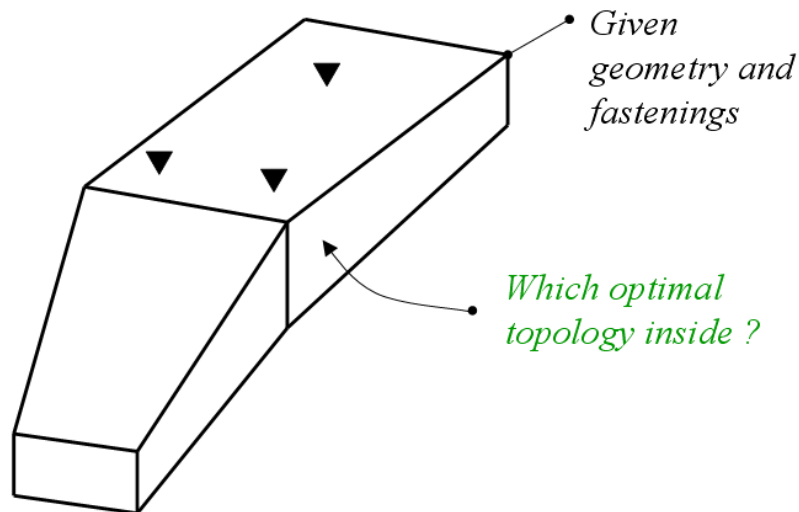
The second design



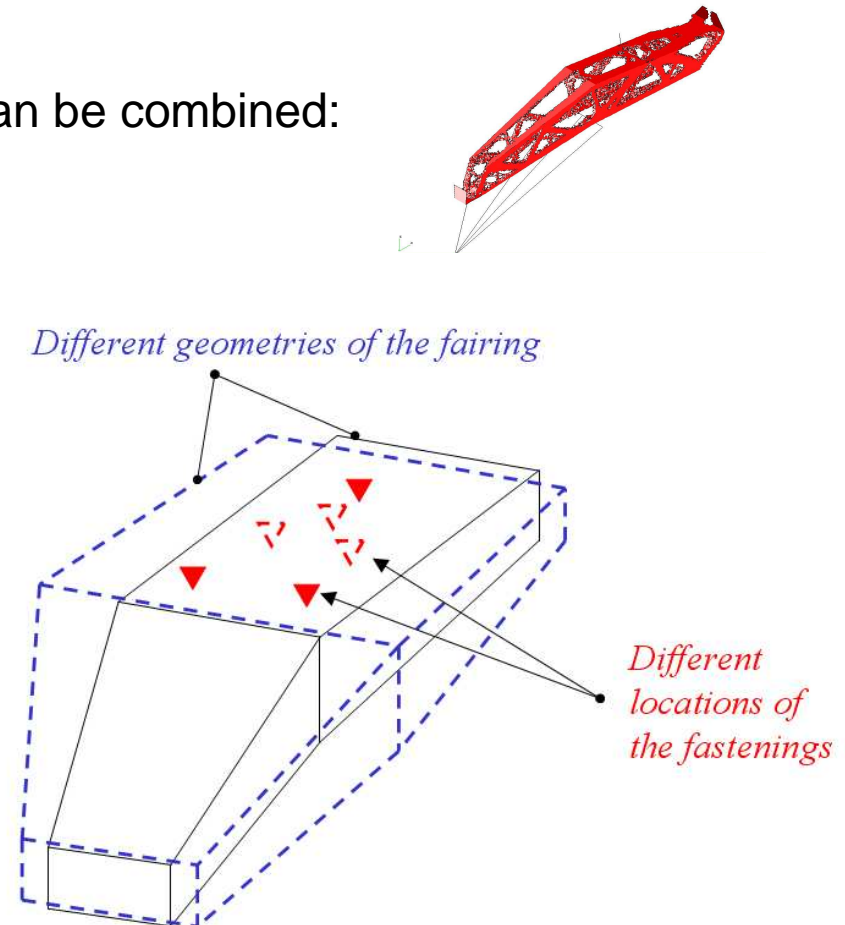
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Problem statement

Two kinds of design variables which can be combined:



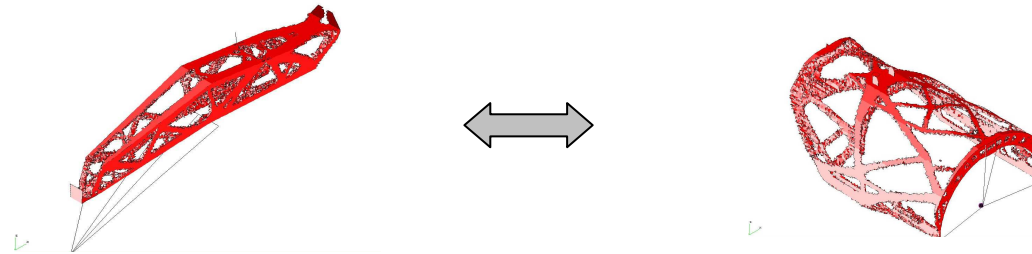
Topology design variables



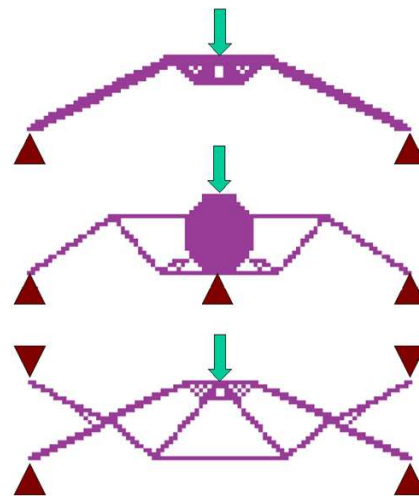
Geometric design variables

Problem statement

- Influence of the geometry on the optimal topology: observed before.

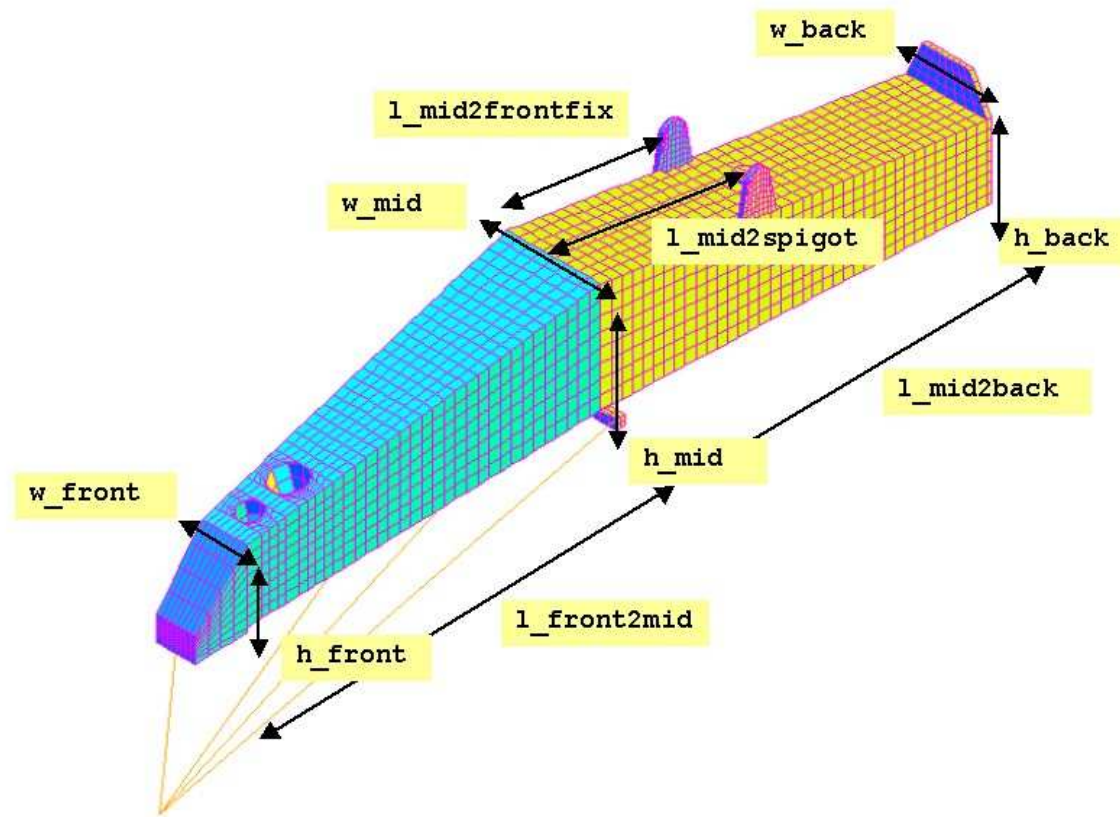


- Influence of the boundary conditions on the optimal topology:



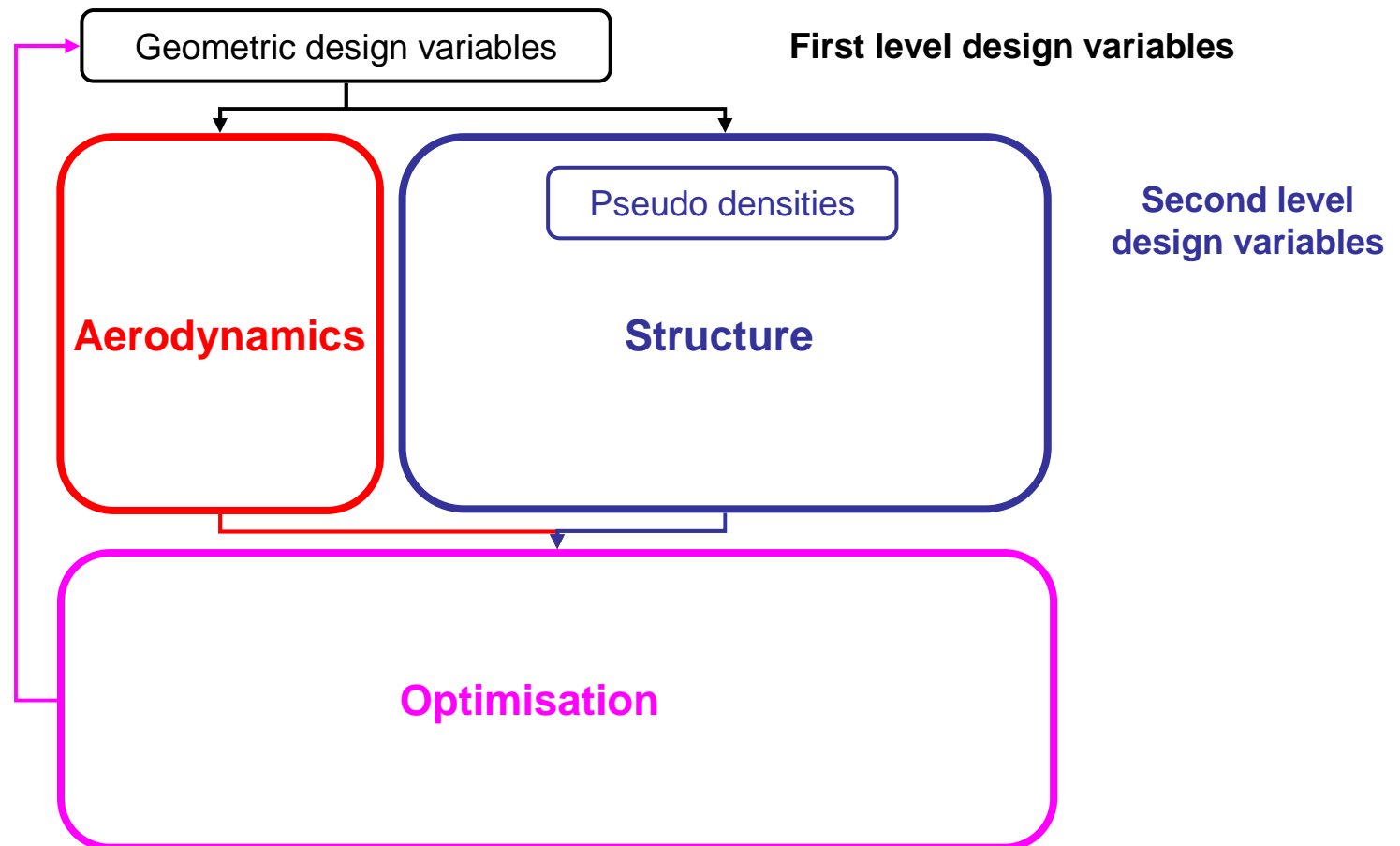
Problem statement

Set of design variables (geometry and fastening):



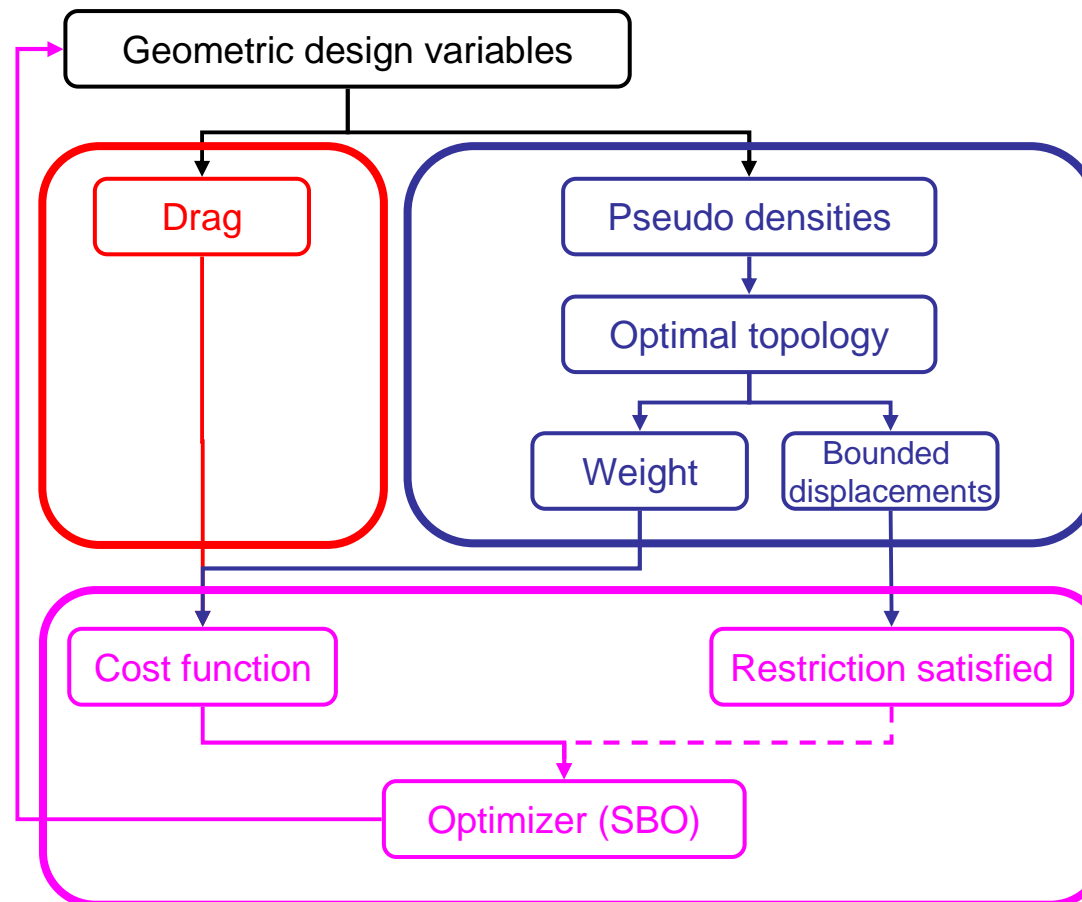
Problem statement

Two disciplines which are considered:



Problem statement

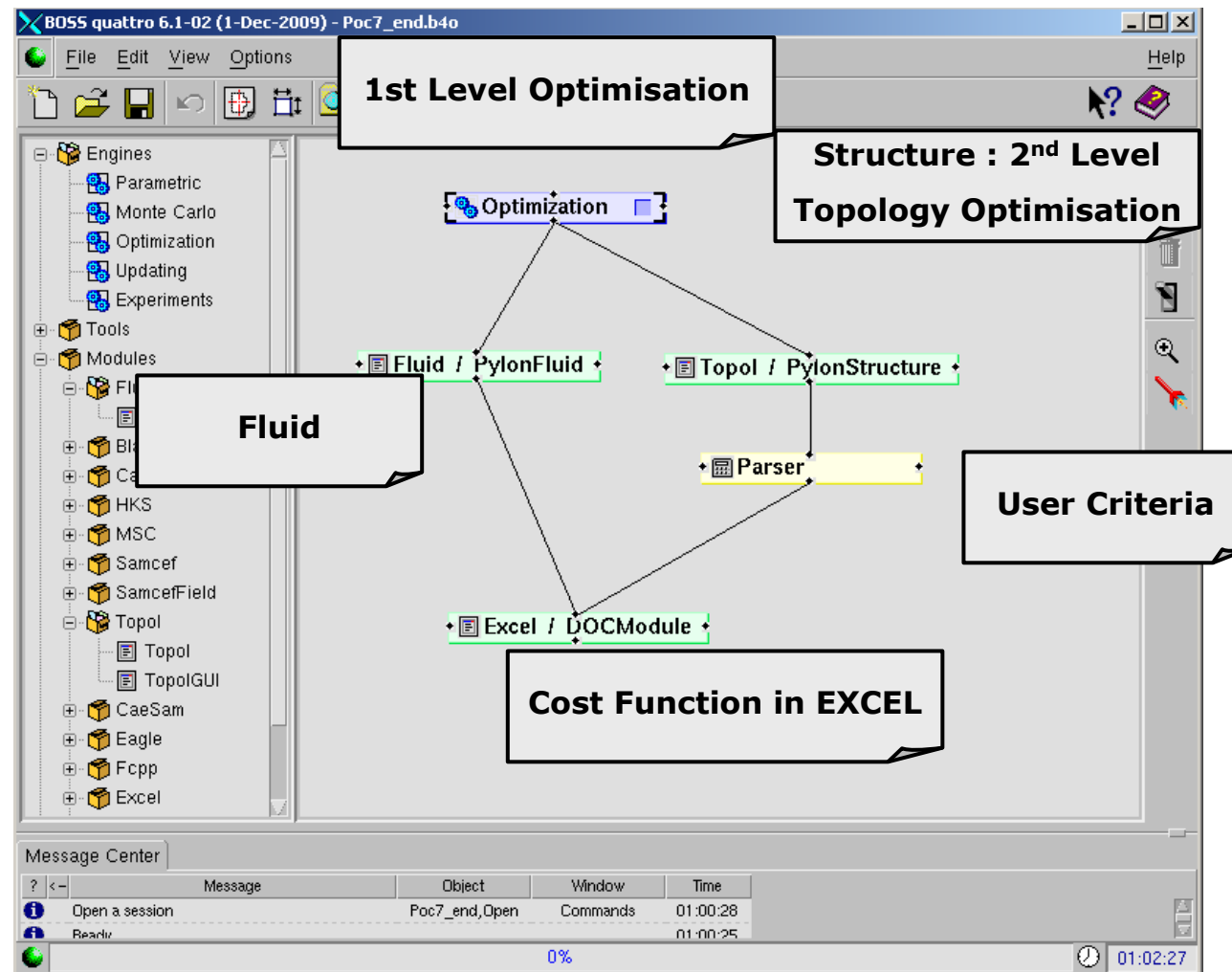
Two disciplines which are considered:



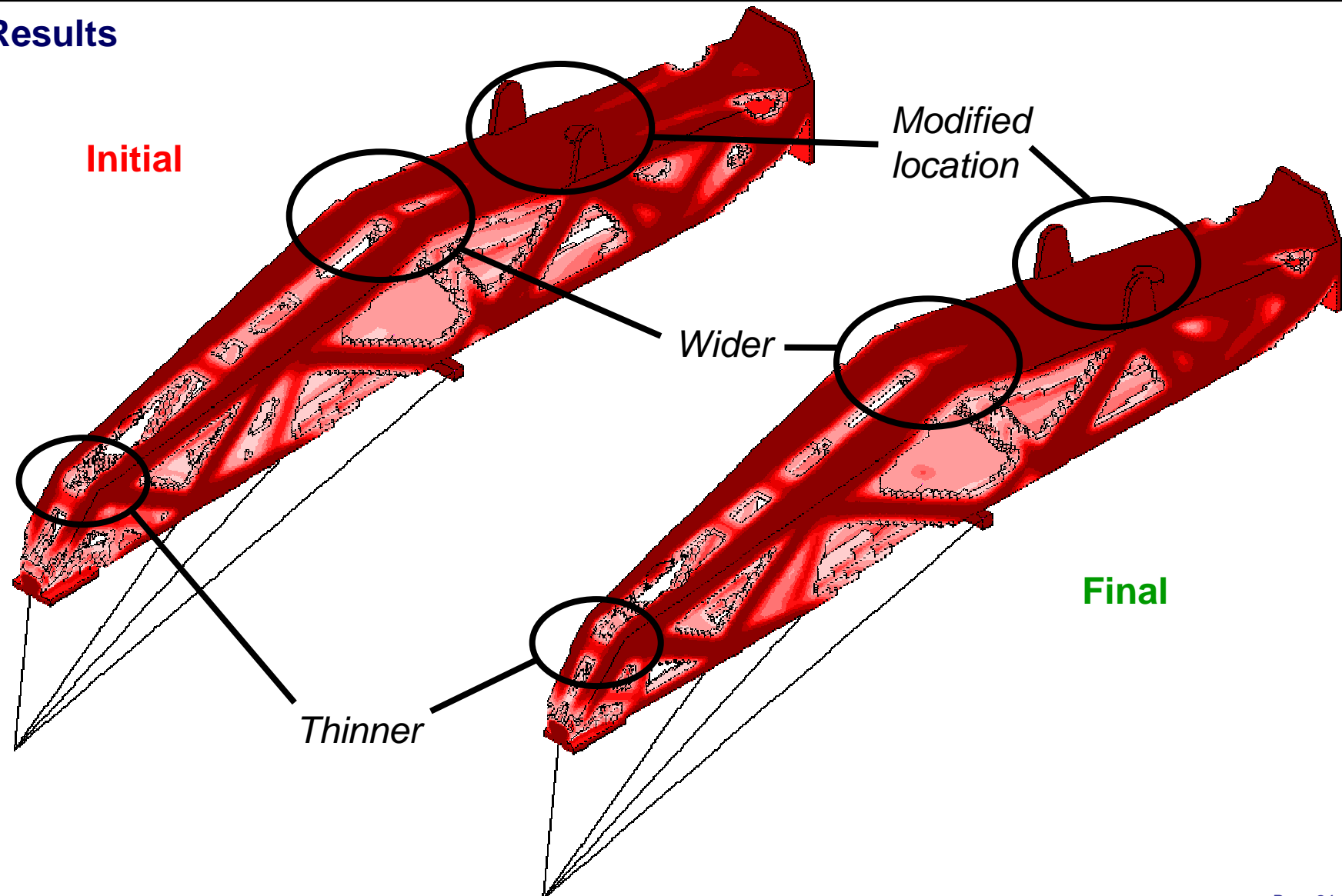
Bi-level optimization



Implementation in the BOSS quattro software

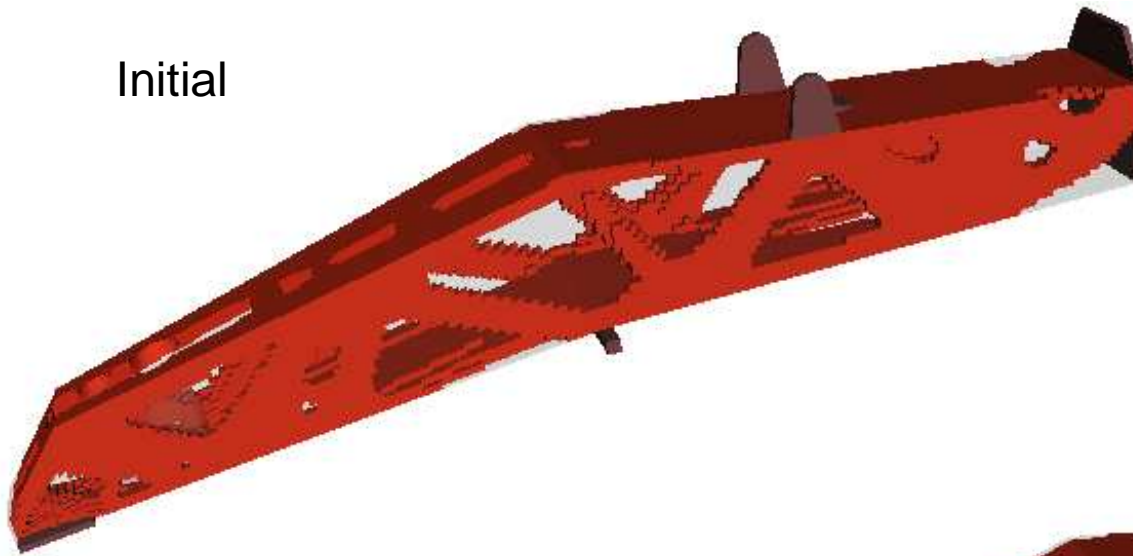


Results

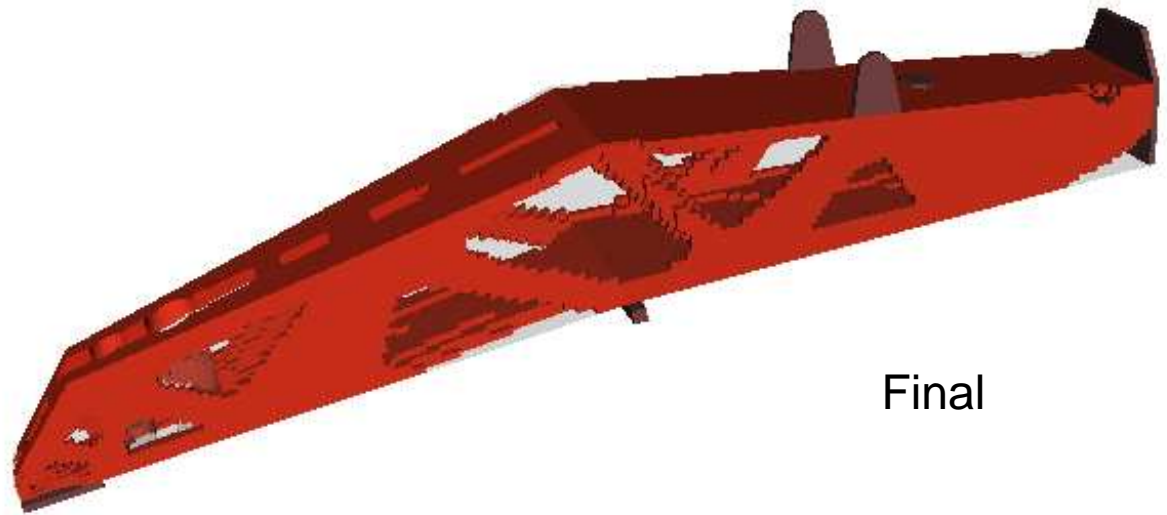


Results

Initial



Final



Conclusions



- Original designs of Airbus pylons have been presented
- Bi-level optimization scheme has been presented
 - includes topology optimization
 - includes shape optimization (+ location of the boundary conditions)
 - multidisciplinary optimization
 - aerodynamics
 - structure
 - demonstrated on an Airbus applications
 - applications with other design problems are being investigated

Acknowledgements



A part of the development of the bi-level optimization approach has been performed within the CRESCENDO project, funded by the European Community's Seventh Framework Programme (FP7/2007-2013) under grant agreement n° 234344 (www.crescendofp7.eu/).